

embodiment, ring gear 80, sun gear 84 and planet gears 82 include double-helical, or herringbone, tooth configurations that facilitate flow of lubrication oil through epicyclic gear system 32.

Ring gear 80 of epicyclic gear system 32 is connected to fan shaft 26 and second-stage shaft 30 through flanged connection 60. Fan shaft 26 is connected to compressor shaft 54 such that fan shaft drives ring gear 80 at the same speed as compressor shaft 54. Likewise, second-stage shaft 30 is connected to second-stage rotor 62 to drive second-stage fan blades 14B at the same speed as compressor shaft 54. Thus, second-stage fan blades 14B are directly driven by compressor shaft 54 without needing to go through a gear reduction system. Ring gear 80 is also directly driven by compressor shaft 54 to drive first-stage shaft 28 through planet gears 82 and sun gear 84. First-stage shaft 28 is connected to carrier 88 with, for example, threaded fasteners at bores 122 of carrier 88 and bores 124 of first-stage shaft 28. In other embodiments, second-stage shaft 28 is connected to carrier 88 using a flexible torque plate coupling in conjunction with bores 122, as is described in U.S. Pat. No. 5,466,198 by McKibbin et al., which is herein incorporated by this reference. As compressor shaft rotates ring gear 80, ring gear 80 spins planet gears 82 around stationary sun gear 84. Planet gears 82 pull gear carrier 88 about axis A in the same rotational direction as ring gear 80, but at a reduced rate. Thus, first-stage shaft 28 is driven to rotate about axis A in the same direction as second-stage shaft 30, but at a slower speed.

Epicyclic gear system 32 achieves a reduction in the rotational speed of first-stage shaft 28 commensurate with optimal operation of two-stage fan section 12. For example, differential gear systems, in which the sun gear, the carrier and the ring gear all rotate, have been employed to rotate counter-rotating fan sections in other gas turbine propulsion systems. Differential gear reduction systems, however, achieve gear reduction ratios on the order of 8:1 or more, which would result in the first-stage fan shaft rotating at about thirteen percent of that of the second-stage fan shaft. In co-rotating, two-stage turbofans, it is desirable that the two fan stages rotate at similar speeds such that mass flows generated by each stage are closely matched. With the gear system of the present invention, in which sun gear 84 is maintained stationary by static torque tube 70, lower gear reduction ratios are attainable, as is illustrated by equation (1), where N_R is the number of teeth in ring gear 80 and N_S is the number of teeth in sun gear 84.

$$\frac{N_R + N_S}{N_R} \quad \text{Equation (1)}$$

In one embodiment of epicyclic gear system 32, the ring gear has 117 teeth, the planet gears have 37 teeth, and the sun gear has 43 teeth such that a gear reduction ratio of about 1.37:1 is achieved. Thus, the rotational speed of first-stage fan shaft 28 is reduced to about seventy-three percent of that of second-stage fan shaft 30, as is illustrated by equation (2), where $\omega_{\text{Second-Stage}}$ is the rotational speed of second-stage shaft 30 and $\omega_{\text{First-stage}}$ is the rotational speed of first-stage shaft 28.

$$\omega_{\text{Second-Stage}} = \omega_{\text{First-stage}} \left(\frac{N_R + N_S}{N_R} \right) \quad \text{Equation (2)}$$

In another embodiment of the invention, the rotational speed of first-stage fan shaft 28 is reduced to about eighty-three percent of that of second-stage fan shaft 30.

Additionally, epicyclic gear system 32 achieves more efficient torque transfer from compressor shaft 54 to first-stage shaft 28 and second-stage shaft 30. Typical counter-rotating fan gas turbine propulsion systems utilize a differential gear system that transfers power from a single rotational input to two rotational outputs. Thus, both power outputs are derived from the gear system, which produces inefficiencies in the power transfer and requires more robust gear systems. Epicyclic gear system 32 of the present invention, however, permits power from compressor shaft 54 to be directly transferred to second-stage shaft 30. Second-stage shaft 30 is directly coupled to compressor shaft 54 through fan shaft 26. Thus, gear reduction inefficiencies only result in transferring power to first-stage shaft 28 from epicyclic gear system 32. Also, since only first-stage shaft 28 receives power from gear system 32, gear system 32 need only be sufficiently robust to transfer a portion of the power of compressor shaft 54, rather than all of the power of compressor shaft 54. This also permits epicyclic gear system 32 to achieve smaller diameters and more compact designs.

Although the present invention has been described with reference to preferred embodiments, workers skilled in the art will recognize that changes may be made in form and detail without departing from the spirit and scope of the invention.

The invention claimed is:

1. A two-stage turbofan system for use in a gas turbine engine through which inlet air travels from an upstream direction to a downstream direction, the two-stage turbofan system comprising:

a second-stage fan shaft for connection with a drive shaft in the gas turbine engine such that the second-stage fan shaft is driven at a speed of the drive shaft;

a stationary torque tube having a fixed upstream portion for connection with a fan case in the gas turbine engine;

a gear system comprising:

a ring gear connected to the second-stage fan shaft;

a stationary sun gear connected to a downstream portion of the torque tube concentric with the ring gear; and

a gear carrier positioned concentrically between the ring gear and the sun gear, the gear carrier having a plurality of planet gears positioned in the gear carrier to interface with the sun gear and the ring gear; and

a first-stage fan shaft having a downstream portion extending from the gear carrier such that the first-stage fan shaft is driven at a speed reduced from that of the drive shaft.

2. The two-stage turbofan system of claim 1 wherein the gear system comprises an epicyclic gear train.

3. The two-stage turbofan system of claim 1 and further comprising a plurality of journal pins positioned within the plurality of planet gears and connected to the carrier.

4. The two-stage turbofan system of claim 3 and further comprising:

an oil manifold connected to the plurality of journal pins; and

an oil feed extending through the stationary torque tube and connecting with the oil manifold.

5. The two-stage turbofan system of claim 4 wherein the plurality of journal pins include radially extending lubrication bores such that oil from the oil manifold can be centrifugally driven from the oil manifold to the interface of the ring gear and the plurality of planet gears.

6. The two-stage turbofan system of claim 5 and further comprising an oil collection system for gathering oil centrifugally passed through the gear system.